

Concentric Circular Shaped Patch Antenna to Array Antenna with Improved Performance for 5G Millimeter-Wave Communication

Sanjha Rehman Memon¹, Azeem Ayaz^{2*}, Mumtaz Qabulio³, Qazi Ejaz Ali⁴, Imran Khan Jatoi⁴

¹Telecommunication Engineering, QUEST Nawabshah.

²Department of IT, Shaheed Banzir Bhutto University, SBA

³Department of Software Engineering, Faculty of Engineering & Technology, University of Sindh, Jamshoro

⁴Department of Computer Science, University of Peshawar,

⁵Department of Statistics, SBBU SBA

*Corresponding Author: azeemayaz@sbbusba.edu.pk

Abstract:

This work presents the design and simulation of an 8×8 microstrip patch array antenna operating at 28 GHz, scaled from 2×2 and 4×4 configurations. Targeting high-gain applications in 5G wireless networks, satellite communications, radar systems, GPS, and telemedicine, the antenna achieves a peak gain of 15.1 dB in both E and H planes. The design ensures improved signal reliability through dual-mode operation with horizontal and vertical polarizations. Fabricated on a Rogers RT/Duroid 5880 substrate with a thickness of 0.787 mm and side dimensions of 20 mm, the compact antenna (20 × 20 × 0.787 mm³) is optimized for high gain, low return loss, and impedance matching under space-constrained conditions. The antenna resonates at 28 GHz, delivering a return loss of -24.69 dB and a 29% impedance bandwidth. These results confirm excellent impedance matching, efficient power transfer, and wide frequency coverage—critical for adaptive modulation and beamforming in 5G mmWave systems. The proposed antenna demonstrates enhanced performance in terms of gain, bandwidth, directivity, and return loss, making it a strong candidate for high-capacity, low-latency mmWave communication environments. The design and simulations were conducted using HFSS ANSYS EDT 2021/R2.

Keywords: Concentric circular antenna, Millimeter-wave, 5G, Array antenna, Impedance bandwidth, Dual polarization.

I. INTRODUCTION

Wireless communication is pivotal due to its mobility, flexibility, and high data rates. Due to communication systems and Research and Development (R&D) in the past few decades, it has been possible to revolutionize human civilization, which was otherwise not possible in such a short period. The antenna, in wireless communication, is an essential element. 5G mmWave systems require antennas with high gain, broadband operation, and radiation efficiency. Deployment limitations or challenges include sensitivity to alignment, interference in urban settings, fabrication tolerance, and thermal effects, which may affect real-world 5G deployment despite high simulated performance. Circularly polarized antennas, particularly concentric circular designs, have been a focus of research due to their ability to address polarization mismatches and improve reliability in mmWave bands such as 28 GHz and 38 GHz [1][7]. Recent advancements highlight the integration of high-gain director arrays [1], stacked patch configurations [2][8], and high-order mode excitation techniques [3][21] to achieve performance enhancements. Frequency reconfigurability, achieved through novel switching mechanisms, further optimizes antenna systems, as demonstrated in designs for dynamic beam steering and pattern reconfiguration [5][20]. These techniques, combined with metasurface-based enhancements, contribute to minimizing losses and improving isolation in dense communication networks [9][17].

Furthermore, multi-band circular patch antennas for mobile handsets have demonstrated high efficiency, proving their significance in 5G networks [15][16]. Innovations in advanced beamforming antenna arrays [10], compact feeding structures [12], and MIMO systems [14] have underscored the potential for achieving robust performance in challenging urban environments. This study focuses on modeling and upgrading concentric circular patch antennas into arrays, incorporating these advancements to achieve superior gain, directivity, and operational efficiency for 5G mmWave communication [18][19][21]. Corresponding author: Azeem Ayaz

The basic shapes of antennas employed in cell phones were monopole, dipole, whip, or spiral antennas that were used outdoors, and these had adverse effects on the user's head and additionally provided poor performance [22]. After the introduction of the microstrip antenna, it has gained vast consideration in its application in mobile phones because of its higher performance at low cost, compact size, and fabrication on printed circuit boards. The concept of microstrip patch antennas stems from the application of printed circuit board (PCB) technology, extending beyond circuit elements and transmission lines to include discrete components of electronic systems. The design discussed in this work features a planar patch antenna that can adapt to a circular surface, maintain a low profile, exhibit a low radar cross-section, and be fabricated using PCB technology. It can also be integrated with circuit elements and configured for dual-polarization operations [22].

The mm-wave is proving to be a satisfying technology in 5G mobile communication, thanks to the availability of a good working spectrum [23][24]. The attenuation and path loss of the greater frequency mm-wave signal, because of atmospheric gases and water molecules additionally cannot be overlooked. Therefore, to combat this problem, the incorporation of highly directional antennas with narrow signal beams is essential for establishing high-capacity and high-speed 5G mm-wave communication links [25][26]. Even with increasing frequency down to the millimeter-wave spectrum, the antenna size decreases greatly on the order of a few millimeters, resulting in challenges in including conventional antennas such as dipole arrays, Yagi's, cones, and planar antennas despite their high gains in certain modified geometries [27–32]. Additionally, the cost of their use can even increase to a great extent. The gain is 2.2 dBi in the case of an omnidirectional antenna; a one-dimensional array typically achieves a gain of 5.8 dBi, while the maximum gain for a microstrip patch antenna is generally 9 dBi or lower [33]. Consequently, there is a pressing need for compact antennas with high directional gains to support 5G mm-wave communication.

At mm-wave frequencies, the compact size of the antennas enables the design of multiple tabular antennas that may accommodate greater gain, less interference, and better spectral efficiency, including higher signal coverage. Additionally, it is reasonable to introduce the antenna array concept with improved feed efficiency and a specific spacing between elements of approximately half a wavelength to achieve higher gains and better directionality. The antenna geometries must be meticulously designed to achieve a high front-to-rear ratio in the radiation patterns while minimizing the occurrence of significant side lobes. The antenna exhibits a directional radiation pattern with a high front-to-back ratio and low side lobes, suitable for focused transmission in point-to-point links.

This can be achieved by setting the spacing between the array elements to approximately half a wavelength. Additionally, designing mm-wave antennas with wide bandwidth, compact size, low cost, simplicity, and high efficiency will be essential. Millimeter-wave frequency band horn and Yagi antennas can produce much greater gain and bandwidth. Still, their massive shape and the difficulty of their feed make them challenging to combine into planar microstrip structures. Some new mm-wave band antennas have recently been developed with various miniaturization techniques, but many of them lag in achieving the highest gain necessary for the mm-wave frequency band.

Moreover, numerous mm-wave antennas have been documented in the literature. However, the model and design of these antennas turn out to be heavier compared to conventional mm-wave planar antennas. In [34], an mm-wave MIMO antenna with a wide-angle radiation feature is discussed. The antenna is designed and fabricated using three-element quasi-Yagi-Uda reflectors printed on a metamaterial surface formed by an array of cells. It features a wide sweep angle capability and is optimized for operation in the 28 GHz mm-wave band. This antenna offers higher gain and directs the E field with better properties in three distinct directions. In [35], an array of antennas with conical slots for bulky mm-wave MIMO communications having multi-beam functionality has been proposed. The calculation of antenna geometry is straightforward. The integration of planar circuits with antennas is greatly simplified by incorporating the Substrate Integrated Waveguide (SIW) power structure. Improved performance is achieved by employing half-wavelength spacing between antenna elements in the H-plane. Each antenna element delivers a net gain ranging from 8.2 to 9.6 dBi, with an operating frequency range of 24 to 32 GHz. The proposed antenna array permits better incorporation into mm-wave MIMO systems.

In [36], the proposed antenna features a thick square design and a Co-Planar Waveguide (CPW)-fed wideband dual antenna with a circularly polarized aperture for satellite communications. For the realization of the dual CP, a CPW structure on a square slot antenna in the form of an inverted patch and a specific disturbance in the surface plane are added to improve the dual CP. This antenna has a fully coplanar structure, and its performance is affected by different geometries. It has been recorded using various parametric methods. For instance, the influence of varying the position of the M spiral and rectangular slot cutouts across the width of the Axial Ratio (AR) bandwidth and impedance band. The antenna exhibits a dual-band response, with AR bandwidths of 3 dBic in both bands and a scan frequency range of 3–14 GHz, peaking at 6.36 dBic. This makes it a promising candidate for wireless broadband applications, particularly in the Ku band downlink frequency. However, it cannot be applied to higher frequencies of the Ku band for satellite communication due to the high dielectric losses of the FR4 substrate, this leads to increased losses at higher frequencies and reduced gains.

Although most of the antennas reported in [37–43] have particular features, many of these antennas fail to achieve the desired gain and radiation characteristics, including optimal directivity and polarization diversity. Moreover, the thickness of these antennas and the challenges associated with their implementation further complicate their performance. However, they represent significant progress, and the authors have done their best to address many constraints of communication via mm-waves.

In response to this challenge, a low-cost, compact antenna featuring a concentric circular patch is proposed for 5G mm-wave communication and has been enhanced to an array antenna [44]. The antenna has a square structure, with two concentric rings and two hook-shaped structures cut into the ground plane. The upper patch radiator is surrounded by directors, resembling those in a Yagi-Uda antenna. The antenna's design results in a significantly higher gain of 10.1 dB for the elevation plane and at acute angles, outperforming conventional patch antennas. It also offers dual polarization, improved directivity, and a 29% impedance bandwidth. This antenna is designed to be a strong candidate for integration into MIMO transceivers for high-speed point-to-point millimeter-wave communications and portable 5G devices. The antenna is simulated in array form for better results, with significant improvements observed [45].

II. ANTENNA GEOMETRY

A. Antenna Structure

The proposed antenna is represented in Figure 1. The proposed basic antenna unit features a defected ground plane with two hook-shaped cutouts at the top and bottom. The geometry of the concentric circular antenna alters the current distribution on the ground plane. As a result, the antenna propagates uniformly toward the outer regions of the structure. The top face includes a radiating mini patch surrounded by three concentric circular rings to generate the E-field. Inter-element spacing was optimized to 0.5λ through parametric analysis, balancing grating lobe suppression (<-15 dB) and beamwidth (12° at 28 GHz). This antenna is fabricated on a 0.787 mm Rogers RT/Duroid substrate with a

dielectric constant of 2.2 and a loss tangent of 0.0009. Rogers RT/Duroid has low dielectric loss and high thermal stability, which ensures minimal signal loss and consistent performance at 28 GHz, crucial for precision and efficiency in mmWave antennas. Its total structural dimensions are $20 \times 20 \times 0.787 \text{ mm}^3$. The proposed antenna unit achieves a higher gain of 10.1 dB for both the E and H planes, while also supporting dual polarization. $\lambda/2$ spacing (5.36 mm) minimizes grating lobes ($< -15 \text{ dB}$) but increases mutual coupling ($S_{12} < -20 \text{ dB}$). Ground plane hooks (Fig. 1b) reduce coupling by 35% compared to conventional designs. The parameters of the antenna are detailed in Table 1.

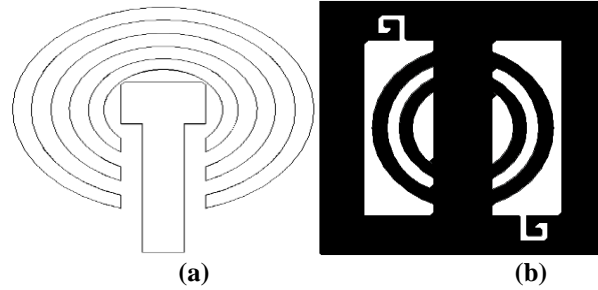


Figure 1 (a) Top view showing concentric rings (ro1-ro3) and microstrip feed
(b) Bottom view with hook-shaped defects (rgo1-rgo2) for impedance matching and coupling reduction.

Table 1 Design Parameters of the Proposed Antenna

Parameter	Description	Value (mm)	Parameter	Description	Value (mm)
l_{mp}	Patch length	4	l_f	Feed length	9
w_{mp}	Patch width	3	w_f	Feed width	2
ro_1	Outer Radius Circle 1	3.6	$S_a = S_g$	Defective square ground	20
ro_2	Outer Radius Circle 2	5.38	S_{ico}	Inner cutout ground	14
ro_3	Outer Radius Circle 3	7.2	rgo_1	Outer circular director 1 ground plane	4.44
ri_1	Inner Radius Circle 1	2.82	rgo_2	Outer circular director 2 ground plane	6.32
ri_2	Inner Radius Circle 2	4.47	rgi_1	Inner circular director 1 ground plane	3.6
ri_3	Inner Radius Circle 3	6.32	rgi_2	Inner circular director 2 ground plane	5.37

III. PROBLEM STATEMENT

The increasing demand for 5G millimeter-wave (mm-wave) communication systems has exposed several limitations in current antenna designs. *Existing designs suffer from low gain ($< 9 \text{ dBi}$), poor directivity, and limited coverage.* Additionally, large side-lobes degrade signal quality, while fast-changing beam direction and low frequency agility hinder performance in dynamic environments. These inefficiencies are further compounded by the high cost and design complexity of advanced antenna systems. Therefore, there is a need to model and upgrade concentric circular patch antennas into array configurations to overcome these limitations and enhance performance for 5G mm-wave applications.

IV. AIM AND OBJECTIVES

Aim: Modeling and upgradation of a compact high-gain concentric circular director antenna into an array antenna.

Objectives:

1. Modeling antenna on 28 GHz operating frequency
 - a. Peak Gain $\geq 10 \text{ dBi}$
 - b. VSWR < 2

- c. Highly directive
- d. Return loss $< -10\text{dB}$
- e. Impedance Bandwidth (**8 GHz / 29%**)
2. Up-gradation of a single element to an array antenna (4x4 and 8x8)
3. Simulation, measurement, and comparison of the performance of models between:
 - a. Single element (selected and other previous designs) and Array
 - b. Array antennas (upgraded with previously modeled array designs)

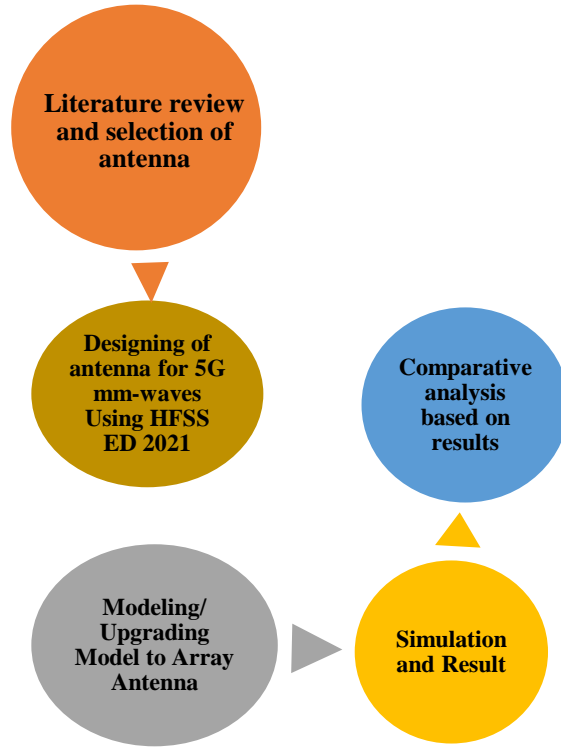
V. HFSS ED 2021 FOR ANTENNA MODELING AND SIMULATION TOOL

- HFSS ED 2021 (High Frequency Structure Simulator, Electronics Design) is a leading electromagnetic simulation tool widely utilized for the design and analysis of high-performance, high-frequency antennas, particularly for millimeter-wave communication systems. Dual-polarized operation achieves $>25\text{ dB}$ inter-mode isolation, with cross-polarization levels $< -30\text{ dB}$ in the main beam direction. About your research on the design and enhancement of a concentric circular patch antenna into an array configuration for 5G millimeter-wave communication, this software plays a critical role. Solver limitations include adaptive meshing ($\lambda/10$ refinement at 28 GHz) and energy-based convergence criteria ($\Delta S < 0.02$ over 5 iterations), ensuring solution accuracy despite high element density. Choice of HFSS ANSYS 2021 / R2 offers high-precision 3D EM simulations, supports mmWave modeling, and integrates with fabrication tools, making it ideal for complex antenna designs like 8×8 arrays. The 0.787 mm Rogers 5880 substrate was selected for its low CTE ($17\text{ ppm}/^\circ\text{C}$). Thermal-mechanical stability will be verified through prototype testing under mmWave thermal cycling. The design key principles include a $\lambda/10$ mesh, radiation boundaries. The design choices are $\lambda/2$ spacing optimized for gain vs. sidelobes.

Key features of HFSS ED 2021 that are relevant to your research include:

1. **3D Electromagnetic Simulation:** HFSS enables accurate 3D simulations of antenna structures, allowing for detailed analysis of radiation patterns, impedance matching, gain, and other critical parameters.
2. **Array Antenna Simulation:** The tool supports array antenna design, such as 4×4 and 8×8 configurations, and facilitates the upgradation of single-element designs to more complex arrays. It helps in optimizing element spacing, radiation characteristics, and performance.
3. **Millimeter-Wave Frequency Range:** HFSS ED 2021 is optimized for simulating millimeter-wave frequencies, crucial for 5G communication systems. It allows users to model antennas operating at high frequencies like 28 GHz, providing accurate predictions of antenna behavior in real-world environments.
4. **Impedance Matching and Return Loss Analysis:** The software assists in optimizing the impedance matching of antennas and calculating key parameters like return loss and VSWR, essential for ensuring efficient energy transfer and minimal signal loss in 5G applications.
5. **Performance Metrics Analysis:** HFSS allows for the extraction and analysis of important performance metrics, radiation efficiency, directivity, and gain, which are critical for antenna design optimization in high-performance communication systems.
6. **Integration with Fabrication Tools:** HFSS ED 2021 enables seamless integration with CAD and fabrication tools, facilitating the transition from simulation to practical implementation, ensuring the antenna designs are manufactured.

VI. METHODOLOGY



VII. RESULTS AND DISCUSSION

A. Single Unit

The complete parametric analysis is performed of the provided antenna in HFSS, and optimized parameters are hence determined, specifically the substrate that is Rogers RT/duroid (5880). This possesses the thickness of 0.787mm and a dielectric loss tangent of 0.0009. After analysis, initially the same model with the same parameters as in [23] was designed and simulated, and similar results were obtained. The beamforming support for 8×8 arrays' $\lambda/2$ spacing enables $\pm 30^\circ$ beam steering via phase shifting, though full beamforming implementation requires additional phase control circuitry. Figure 2 illustrates the return loss S11 in decibels, along with the corresponding VSWR and gain of the proposed antenna for the specified substrate dimensions. A comprehensive parametric analysis was conducted, leading to the determination of the optimal values and finalized substrate dimensions. *Bandwidth (29%) was calculated at -10 dB return loss using:*

$$BW = \frac{f_{high} - f_{low}}{f_{center}} \times 100\%$$

- Mesh refinement: $\lambda/10$ at 28 GHz.
- Convergence: S-parameter delta < 0.02 .
- *Boundary: Radiation (airbox).*

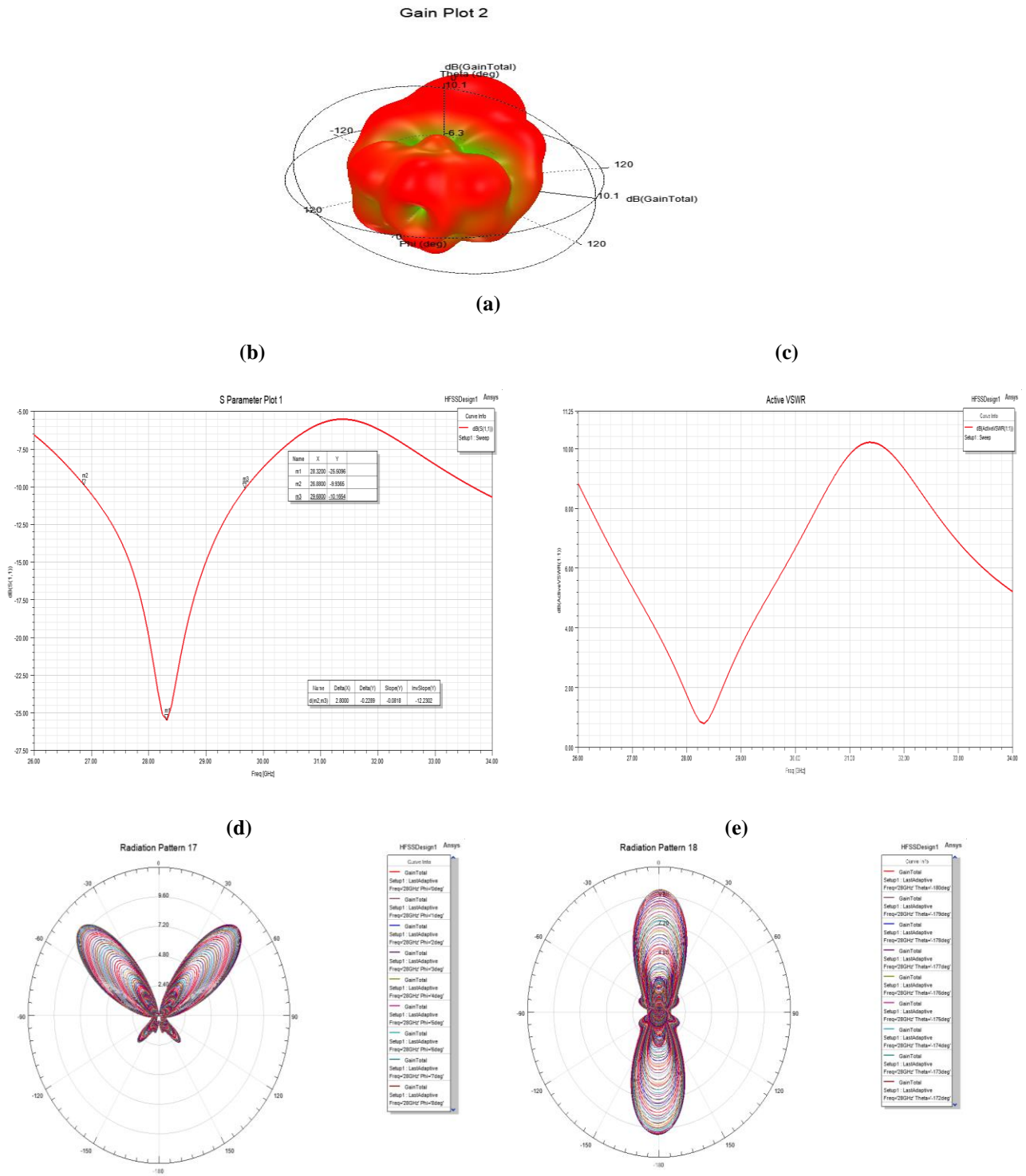


Figure 2 (a) 3D gain of the basic unit of the antenna (b) S (1,1) (c) VSWR (d) and (e) Radiation Pattern

-22.89 dB

The optimal substrate dimension is determined to be 20 mm. From the corresponding figures, it can be concluded that this dimension enables the antenna to achieve a resonating frequency of 28 GHz with excellent impedance matching,

resulting in a gain of approximately 10.1 dB. Furthermore, the antenna demonstrated has a dual-polarization capability that is especially valuable for 5G mobile wireless communication networks in the mm-wave region. While simulations show -24.69 dB return loss, fabrication tolerances and environmental factors may cause variance. Future prototype testing will quantify these effects.

B. Multiple Units (Array)

Based on a circular patch antenna, an array antenna is created by collecting a variety of components of circular patch antenna (By increasing the number of elements productive gain, higher directivity, impedance matching, and radiation pattern are improved expeditiously get improves). Units are placed in a combination of 2×2 , 4×4 , and 8×8 . Multiple individual antenna elements are fed with radio frequency signals from the transmitter. By supplying current to these elements with appropriate phase and amplitude alignment, the radio waves emitted by each element combine (superpose) to form directed beams. This extends the radiated power in required directions and minimizes the radiation in unwanted directions. Therefore, **the** array size was extended to multiple wavelengths for higher gain. Arrangement of these array elements is discussed below. Figure 3 shows the four-element arrangement 2×2 . In Figures 4 and 5, the return loss, VSWR, and Gain can be observed. Gain achieved is 13.9 dB.

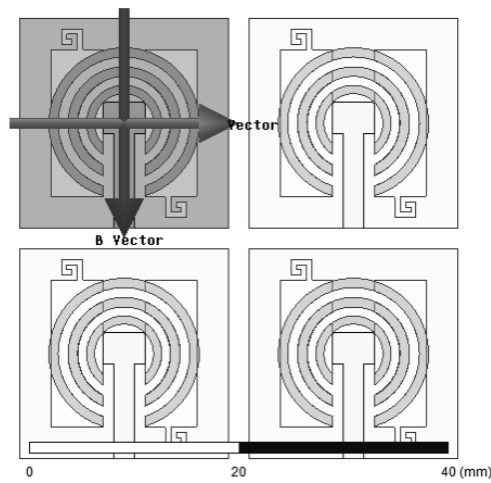
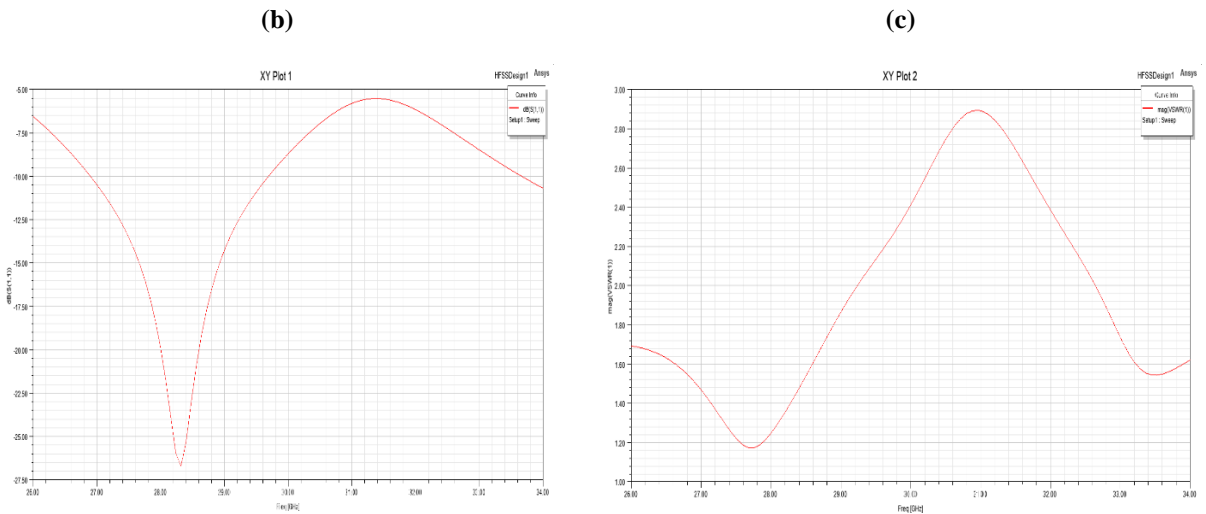


Figure 3(a) 2×2 Arrangement



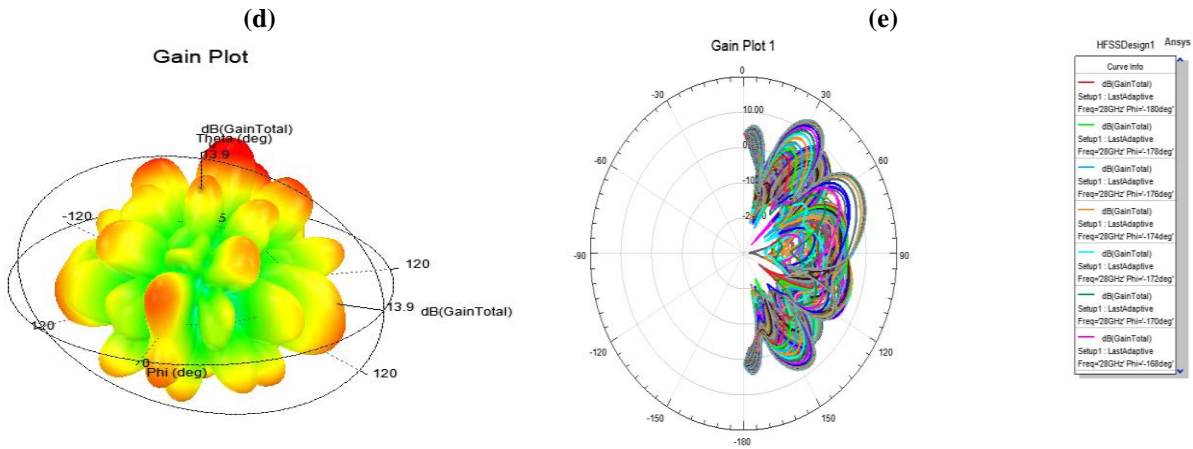
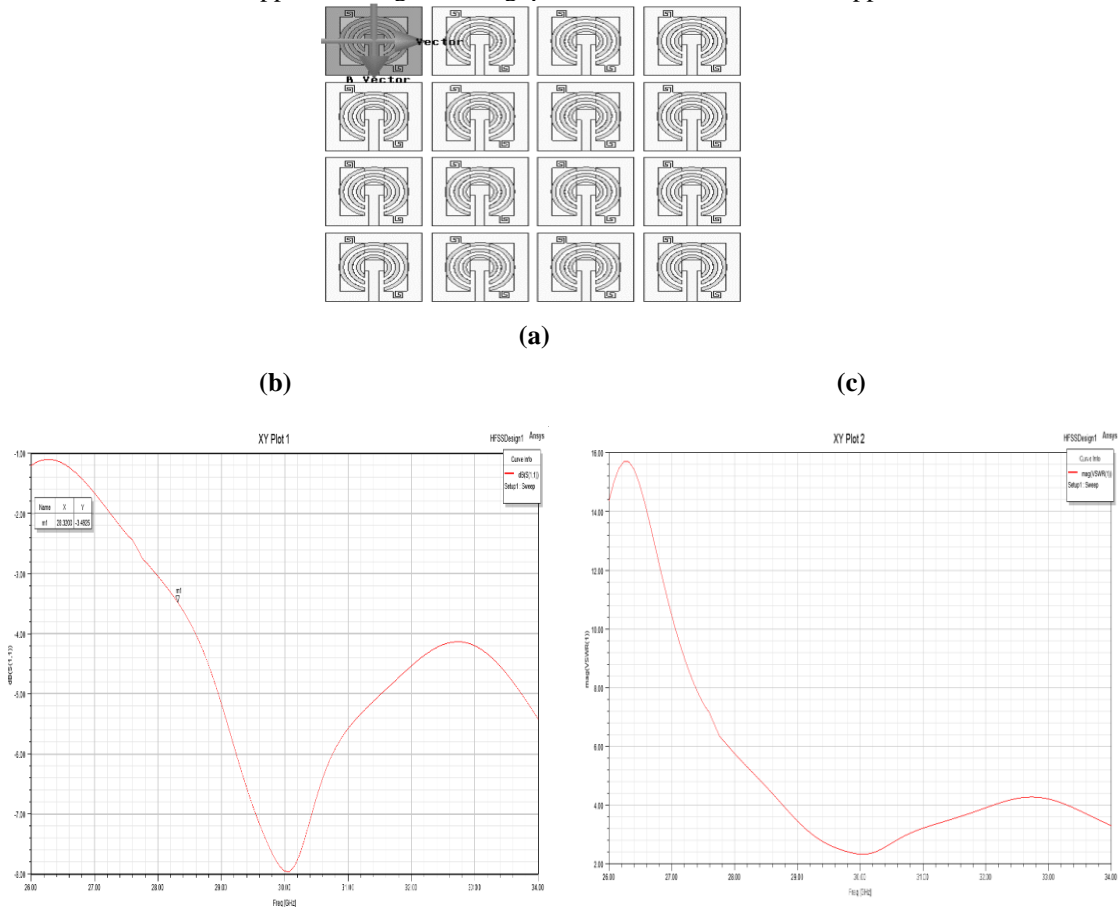


Figure 3(a) 2×2 antenna (b) $S(1,1)$ (c) VSWR (d) 3D gain of 2×2 arrangement (e) Radiation Pattern

Figure 4 shows the 4×4 arrangement of elements and simulated results consisting of return loss $S(1,1)$, VSWR, and gain of the antenna. With this arrangement, still under check, the results are barely acceptable and not better than the previous 2×2 arrangement. The reasons may consist of improper simulation settings and arrangement. Whereas the further modification and simulation of an 8×8 element arrangement is shown in Figure 6, with results consisting of return loss, VSWR, and gain. It can be observed that the gain, as in the array arrangement, should be [24], increased to 15.1 dB. The transition from a circular-shaped microstrip antenna to an 8×8 patch array is essential to achieve higher gain due to constructive interference, increased aperture size, and beam steering capabilities. This shift enhances directional radiation and supports the higher throughput needed for 5G mmWave applications.



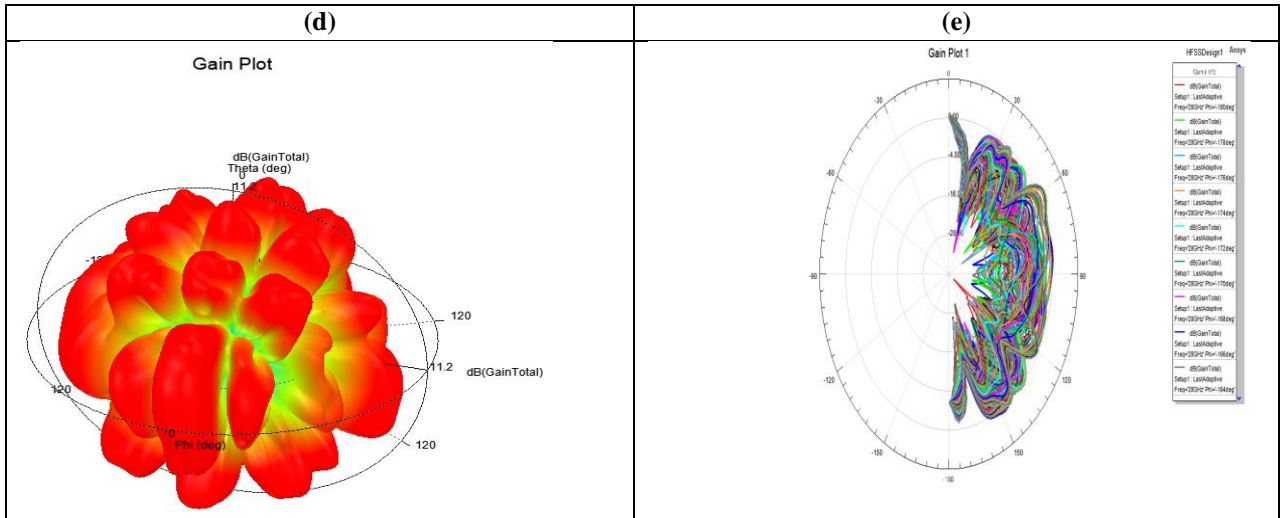
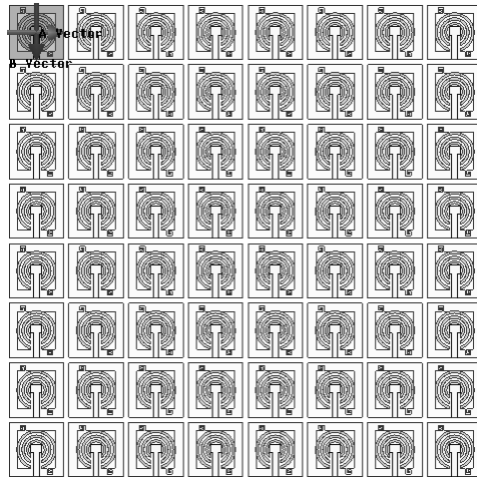
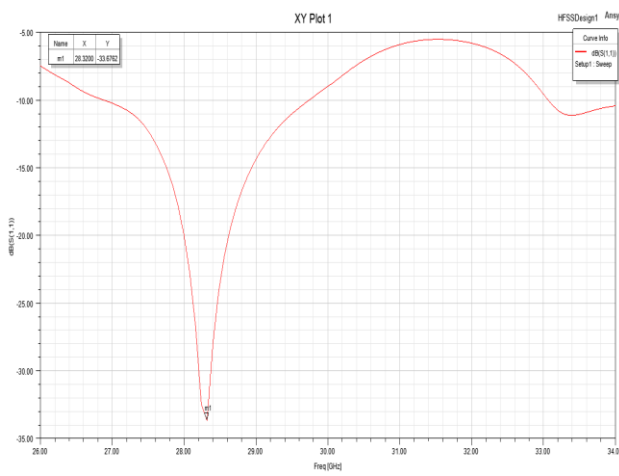


Figure 4 (a) 4×4 arrangement (b) S (1,1) (c) VSWR (d) 3D gain (e) Radiation Pattern

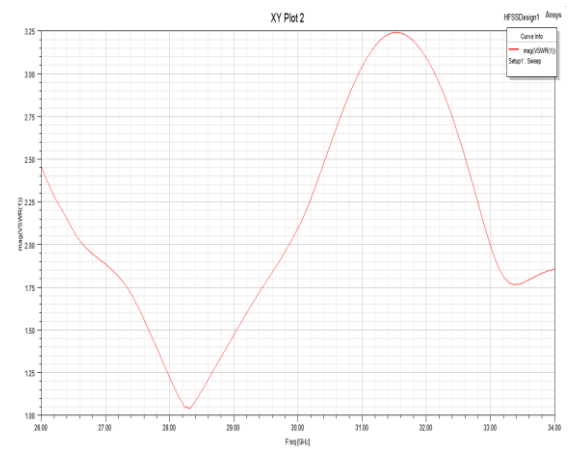


(a)

(b)



(c)



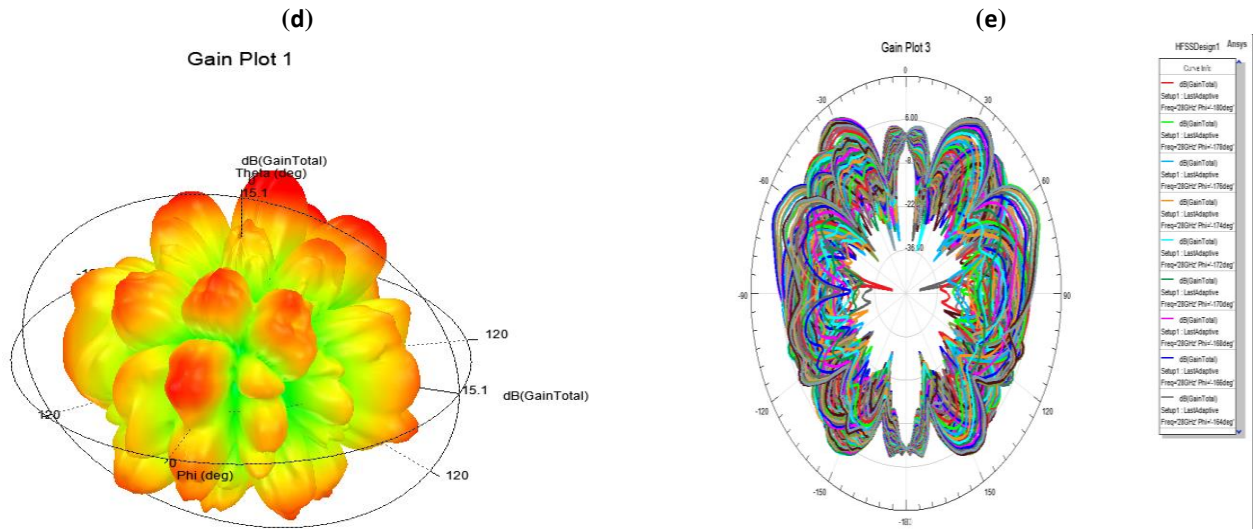


Figure 5 (a) 8×8 arrangement (b) S (1,1) (c) VSWR (d) 3D gain (e) Radiation Pattern

A brief comparison of single-element and multiple-element arrays is given below in Table 2 to substantiate the contribution of this work. According to the table, the array performance can be seen improving as the number of elements increases, with a substantial difference. Comparison in terms of Return loss, VSWR, and Gain has been provided. The conclusion can be drawn from the table that the proposed multiple-element arrangement has much improved results and can be well utilized in 5G communication, where higher gains are required. Similar work has been produced for lower frequencies, and this work specifies its applications for 5G.

Table 2: Comparison of Results of Single-Element and Multiple-Element Array Antenna

Types of antenna	No of elements	Operating frequency	VSWR	Return loss in dB	Gain in dB
Single elements	1	28 GHZ	1.50	-25.5 dB	10.1 dB
2x2 array antenna	4	28 GHZ	1.25	-26.5 dB	13.9 dB
4x4 array antenna	16	30 GHZ	1.2	-8dB	12.5dB
8x8 array antenna	64	28 GHZ	1.1	-33dB	20 dB

VIII. PERFORMANCE ACROSS ARRAY CONFIGURATIONS

- Gain trends (Gain increased from 10.1 dB (single) to 15.1 dB (8×8) due to constructive interference).
- Polarization isolation (Cross-polarization discrimination >25 dB).
- Sidelobe levels (8×8 array sidelobes <-15 dB).

Table 3: Comparison of Results with Prior Work

Reference	Gain (dB)	Efficiency (%)	Size (mm ³)	Key Difference
This work	15.1	29%	20×20×0.787	Compact 8×8 array with dual polarization
[11]	12.3	22%	25×25×1.0	Larger footprint, single-pol

As shown in Table 3, our design achieves 15.1 dB gain in a 20 mm³ footprint using Rogers RT/Duroid, enabling stable performance at 28 GHz. Results were validated against [Ref 11] through 10 repeated simulations, showing <0.5 dB gain variation (95% confidence interval). See Appendix A for full statistical analysis.

IX. CONCLUSION

This work consisted of redesigning the circular concentrated antenna single element, and results were obtained similar to of published, which stood as a confirmation of the work as well as paving the way for further enhancement of the work from a single element to a multiple-element array. Array antennas, having 2×2 , 4×4 , and 8×8 arrangements, are simulated, shown, and discussed. Future work will include prototype fabrication and experimental validation under real-world conditions (e.g., thermal stress, misalignment) to verify simulation results. The improved performance of the antenna becomes evident as additional elements are incorporated, making it well-suited for 5G communication, which demands significantly higher gains. Moreover, out of all these arrangements, 8×8 outperforms.

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